



AVT-371 Research Workshop on

"Materials and technologies for electro-optical camouflage"

Directional thermal infrared emissivity materials and materiel Eoin O'Keefe, QinetiQ, United Kingdom

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- Introduction
 - The thermal infrared threat
 - Field Deployable Electro Optic sensor (FDEOS) kits
 - > The physics (and the problem) of thermal IR emissivity control
- Directional thermal IR emissivity
 - Materials
 - Modelling
 - Combat Identification case
- Summary & questions



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Opens the battlespace to BLUEFOR manoeuvre

Peer REDFOR : A sovereign nation state with Armed Forces whose capabilities [technological, equipment, doctrinal, organisational] are equivalent or superior.

- Increases Detection range over-match
- Reducing signature can increase smoke/obscurant/countermeasure effectiveness

EO CCD : Electro-Optic Camouflage, Concealment & Deception AVT-RWS-371 © QinetiQ 2023 NATO UNCLASSIFIED + EOP

BLUEFOR : Own forces and allies OODA : Observe, Orient, Decide, Act

ISTAR: Intelligence Surveillance Target Acquisition and Reconnaissance

Integrated survivability

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- Peer REDFOR* likely to use layered ISTAR* to control and effect Fires ٠
- BLUEFOR may counter layered ISTAR fire control with Integrated . Survivability - a Layered Strategy
 - Layered Survivability Sometimes called the "Survivability Onion"

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- Electro-Optic (EO) Camouflage Concealment and Deception disrupts ٠ REDFOR OODA* loop at the first stage: degrading 'observation'
 - Reduces REDFOR combat efficiency & interrupts flow of 'kill chain'
- EO CCD is effective at several stages of Layered Survivability Strategy •
 - Reducing probability or range of Detection, Recognition and Identification
 - Enables greater freedom of movement without being detected

- Layered Survivability
 - 1. Don't be there
 - 2. Don't be seen
 - 3. Don't be acquired
 - 4. Don't be hit
 - 5. Don't be killed
 - 6. Do get home

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EO CCD assists 1-4 EO CCD assists 6 too

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'Hemispherical' thermal IR threat direction

Zastava

ISTAR Imaging systems are deployed on UAVs, manned aircraft and other vehicles, and are also used by dismounts.



Takhion



Granat-4



Forpost





Forpost/Israeli optics (2014)



CHN TIR binoculars (2018)









Thermal IR threat evolution



Orlan 30 recce variant with Electro-Optic turret (Ukraine conflict 2022) <image>

GOES-4 produced by NPP AME (RUS) for Forpost R: cooled MWIR WFOV and NFOV, low light TV, range finder & designator HTEB.461321.011 range finder & designator produced by Quantum Optics (RUS)





Thermal IR threat evolution





Left; Orlan 10 recovered in UKR in 2022, Right; close-up of TIR-only imaging pod on recovered Orlan 10

ACTPOH-64012

ТЕПЛОВИЗИОННЫЕ ДЕТЕКТОРЫ



Технология микроболометров: VOx.
Шаг матрицы: 12 мкм.
Спектральный диапазон: 7–14 мкм.
Чувствительность: ≤ 40 мК (@ f / 1,0; 50 Гц; 300 К).
Разрешение детектора: 640 × 512.
Частота кадров: ≤ 60 Гц.

Микроболометрический матричный детектор

ACTPOH-640/75



ТЕПЛОВИЗИОННЫЕ МОДУЛИ С ОБЪЕКТИВОМ

Матричный неохлаждаемый модуль

•Детектор: МФПУ АСТРОН-64017.

•Шаг матрицы детектора: 17 мкм.

 Чувствительность детектора: < 60 мК.
 Чувствительность, температурный эквивалент шума модуля: < 55 мК с технологией снижения шума.

•Разрешение модуля: 640 × 480 (PAL).

•Частота кадров модуля: 25 Гц.

•Спектральный диапазон: 7–14 мкм.

•Автоматическая регулировка усиления. •Цифровое улучшение деталей изображения. •Автоматическое изменение динамического диапазона.

•Настройка параметров через пользовательское меню.

•Объектив: монокристалл германия f/F = 75/1,0. •Серийное производство.



640*480

OSD

Тепловизионные неохлаждаемые модули АСТРОН-640/75 являются базовыми элементами для тепловизионных приборов и аппаратуры. Модули могут быть использованы при разработке и производстве оптико-электронных приборов с тепловизионным каналом разрешением 640 × 480 и углом поля зрения 8,3 × 6,2 градусов. Модуль включает ТВМ АСТРОН-640В17 и объектив АСТРОН-75Ф10. Дополнительную информацию можно получить в разделах с каталожными листами соответствующего модуля и объектива.

Модуль поставляется в полной заводской готовности. Завершающей стадией производства является калибровка тепловизионного модуля с конкретным объективом. Этим достигается наилучшее качество изображения в сравнении с применением модуля без калибровки под конкретный объектив. Особенно это актуально для объективов сдлинным фокусом.

Интеграция модуля в корпус прибора производится через фланец с герметизирующей прокладкой. Параметры питания и выходные сигналы модуля по требованию заказчика могут быть изменены на параметры, указанные на странице «Таблица интерфейсных плат» в разделе «Тепловизионные модули». Производятся серийно.

ГАБАРИТНЫЙ ЧЕРТЕЖ И РАЗМЕРЫ



Фотоприемное устройство АСТРОН-64012 дальнего инфракрасного (тепловизионного) спектра излучения изготовлено на основе матрицы микроболометров с малым шагом. Инфракрасные детекторы с шагом матрицы 12 мкм относятся к последним техническим достижениям в своем классе приборов.

ФПУ АСТРОН-64012 можно отнести к особо перспективным для применения в носимых тепловизионных системах, а также для применения на борту беспилотных летательных аппаратов. Малый геометрический размер матрицы позволяет существенно снизить массогабаритные характеристики оптической системы при сохранении высокого разрешения и чувствительности. Кроме этого, дектор обладает наименьшим энергопотреблением и весом в линейке наших приборов.

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Thermal IR threat evolution

Serial	Year	Chronology of known COTS CHN LWIR portable micro-bolometers			
0	2011	Micro-bolometer array manufacturing established (Yantai, Shandong Province, CHN)			
			Detection ¹ (m)	Recognition (m)	Identification (m)
1	2013	Published: CHN 25 micron pitch, NETD 75mk, fl 40mm, F1 optics	1,200	500	300
2	2015	Published: CHN 17 micron pitch, NETD 50mk, fJ 40mm, F1 optics	1,700	700	500
3	2018	CHN 518B: 17 micron pitch, NETD 50mk, f] 50mm, F1 optics	2,100	900	600
4	2021	CHN TN650: 12 micron pitch, NETD 30mk, fl 50mm, F1 optics	2,800	1,200	800
5	2022	CHN RAPTOR: 12 micron pitch, NETD 20mk, fJ 50mm, F0.9 optics	2,900	1,250	850
6	2023	CHN: 12 micron pitch LWIR Bolometer, NETD 20mk, fl 75mm, F1 optics	4,300	1,800	1,200
7	2024?	CHN current fixed position product, potential to be Field Deployed: 8 micron pitch, NETD 20mk, fi 75mm, F1 optics	5,300	2,300	1,600

¹ Detection, Recognition and Identification of a man-sized object (1.8m) at 20+/-3° °C in a 15 +/-3°C environment calculated with NV-IPM using a MODTRAN standard atmosphere with no precipitation, clouds or aerosols.



Calculated detection probability vs range to target

---- D (2) V50 ---- R (7.5) V50 ---- I (13) V50



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FDEOS

- Field Deployable Electro-Optic Sensor (FDEOS) 'kits'
 - Variants have been produced to help troops understand their EO signature & optimise counter surveillance control measures
 - Indigenous Russian Gen 2+ & Gen 3 Image Intensifier imaging sensors
 - Indigenous Chinese thermal IR imaging systems
 - Other imaging systems









The physics (and the problem) of thermal IR emissivity control

- Match the thermal IR radiance of the platform to the background viewed by the threat
 - Match actual surface temperature to background (conceal hot parts, insulation, solar heat rejection coatings etc. etc.)
 - Minimise remaining radiance contrast using thermal IR emissivity control

Planck

NATO

$$M_{\lambda} = \frac{2\pi c^2 h}{\lambda^5 (e^{hc/\lambda kT} - 1)}$$

Stefan-Boltzmann

 $M(\varepsilon)_{total} = \varepsilon_{total} \sigma T^4$



- Physics 'easy' to solve
 - 'consider a uniform isothermal spherical body in an isothermal environment'
 - Real world much harder
 - > No isothermal simple-shaped bodies or isothermal environments
 - Reducing thermal IR emissivity increases thermal IR reflections
 - Reflected thermal IR radiance can dominate signature
 - Ensure that reflections don't break your camouflage
 - Options for controlling reflected IR radiance:
 - Specular Diffuse surfaces
 - Directional surfaces Control what is reflected in which direction

M = Excitance, λ = Wavelength, c = Speed of light, h = Planck's constant, k = Boltzmann constant, T = Temperature, ε = Emissivity, σ = Stefan-Boltzmann constant, α = Absorptivity, **R** = Reflectivity.

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Directional thermal IR emissivity

- Materials
 - Isotropic reflection
 - Specular to diffuse
 - Directional materials
- Modelling
 - Modelling directional materials
- Combat Identification: co-operative marking case
- Summary



Specular to diffuse

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Paints and metallised grit papers of different roughnesses were characterised on a ZeMetrics ZeScope white light interferometer to estimate their RMS roughnesses and correlation lengths.

Hemispherical Directional Reflection (HDR) were characterised on a SOC-100: specular and diffuse components of reflection were calculated at a range of reflection angles.





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Metallised grit papers (TIR)







Averaged specular and diffuse reflectance at 60° over 8-12µm as a function of RMS roughness







Directional materials – an example







Thermal IR reflective surface Nano-replicated microstructure Polymer web

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Directional materials – what they do



Directional flat quadrants, clockwise from top left:

Foreground	180°, beach shingle
Zenith	0°, clear sky
Right	90°, sea
Left	270°, beach shingle



Three objects:

- specular mirror double curve (spherical Rh mirror)
- directional single curve (vertical axis of symmetry)
- directional flats

Note that sun reflection is absent from the sphere in the LWIR image





Directional materials – what they do



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Modelling directional materials

Inputs:

- Micro-structure facet angles
- Facet emissivities
- Colour layer optical properties
- Surface temperature
- Environment temperatures
 - Statistical
 - Radiometric imagery (spherical mirror)
- Observer position
- Surface position
 - Pitch, roll, yaw

Output:

• Apparent temperature of surface









Modelling directional materials to control contrast radiant intensity (CRI)

Apparent temperature LWIR (8-12µm) predicted with: Temperature of the outer garments 25°C, exposed skin 36°C ambient air and horizon 10°C, sky zenith -20°C



Right-half of the figure treated with a Lambertian surface emissivity of 0.65.

Figure treated with a ground-orientated coating with an emissivity of 0.21.

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CRI 135.6 W sr<sup>-1</sup>
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CRI 209.4 W sr⁻¹





Combat Identification: co-operative marking case







Conformal or 'filling' colour layer Thermal IR reflective surface Nano replicated microstructure Polymer web Adhesive layer





Combat Identification co-operative marking case



8-12 micron image of horizon to 30° elevation

Recorded apparent sky temperature with elevation➢ At high elevation angles, the sky is very cold





Combat Identification co-operative marking case



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-46.1





Combat Identification co-operative marking case



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Combat Identification co-operative marking case







Summary

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- I hope that I have shown you:
 - > The thermal IR threat posed by peer & near-peer adversaries is current & evolving
 - > CCD is a significant part of Integrated Survivability, the thermal IR increasingly so
 - FDEOS kits help troops to understand & optimise counter surveillance control measures
 - Controlling thermal IR emissivity can reduce susceptibility to detection by thermal IR sensors
 - Uncontrolled reflections can impair thermal IR camouflage effectiveness
 - Directional materials can be used to minimise this impairment
 - Application of thermal IR directional materials as a cooperative combat marking material has been discussed
- Finally: there are many variations of directional materials and platform fits that can be considered. It is up to the intelligent camouflage designer to optimise the outcome.